

RL78/G24

120-degree conducting control for permanent magnetic synchronous motor

Summary

This application note explains the sample programs driving a permanent magnetic synchronous motor in the 120-degree conducting method using the RL78/G24 microcontroller. This note also explains how to use the motor control development support tool, 'Renesas Motor Workbench (RMW)'.

These sample programs are intended to be used as references only, and Renesas Electronics Corporation does not guarantee their operation. Please use them after carrying out a thorough evaluation in a suitable environment. Working in a high voltage environment is dangerous, so please read the user's manual for each development environment carefully before using the product in consideration of safety. Renesas cannot be held responsible for any accidents or damages that may occur in the development environment listed in this application note.

Operation checking device

Operations of the sample programs have been checked by using the following device.

• RL78/G24(R7F101GLG2DFB)

Target sample programs

The target sample programs of this application note are as follows.

- RL78G24_MCEK_120_CSP_CC_V100 (IDE: CS+ for CC)
- RL78G24_MCEK_120_E2S_CC_V100 (IDE: e²studio)

Reference

- Application note: '120-degree conducting control of permanent magnetic synchronous motor: algorithm' (R01AN2657EJ0120)
- RL78/G24 Group User's Manual: Hardware (R01UH0961EJ0110)
- Renesas Motor Workbench 3.1.2 User's Manual (R21UZ0004EJ0402)
- RL78/G24 Motor Control Evaluation Kit User's Manual (R12UT0021EJ0100)

Contents

1. Overview

This application note explains how to implement the 120-degree conducting control sample programs of permanent magnetic synchronous motor (PMSM) using the RL78/G24 microcontroller and how to use the motor control development support tool, 'Renesas Motor Workbench'. Note that this sample programs use the algorithm described in the application note '120-degree conducting control of permanent magnetic synchronous motor: algorithm'.

1.1 Development environment

Table 1-1 and [Table 1-2](#page-2-1) show development environment of the sample programs explained in this application note.

For purchase and technical support, please contact sales representatives and dealers of Renesas Electronics Corporation.

Notes:

- 1. The RL78 / G24 CPU CARD (RTK0EMG240C00000BJ), Inverter board (RTK0EMGPLVB00000BJ) and communication board (RTK0EMXC90Z00000BJ) are products of Renesas Electronics Corporation.
- 2. TG-55L is a product of TSUKASA ELECTRIC. TSUKASA ELECTRIC. (https://www.tsukasa-d.co.jp/en/)

2. System overview

An overview of this system is provided below.

2.1 Hardware Specifications

RL78/G24 Motor Control Evaluation Kit (RTK0EMG24SS00000BJ) consists of Inverter board, CPU board, and communication board. Each specification is shown below.

Table 2-1 Specifications of RL78/G24 Motor Control Evaluation Kit (RTK0EMG24SS00000BJ)

Table 2-3 Specifications of RL78/G24 CPU Card (RTK0EMG240C00000BJ)

Table 2-4 Specifications of Communication board (RTK0EMXC90Z00000BJ)

2.2 Hardware configuration

The hardware configuration is shown below.

Figure 2-1 Hardware Configuration Diagram

2.3 Hardware specifications

2.3.1 User interface

[Table 2-5](#page-8-0) is a list of user interfaces of this system.

The connector interfaces of this system are listed in [Table 2-6.](#page-8-1)

Table 2-6 CPU Card Connector Interfaces

This jumper setting of this system is listed in [Table 2-7.](#page-8-2)

Table 2-7 Jumper settings

[Table 2-8](#page-9-0) is a list of port interfaces of RL78/G24 microcontroller of this system.

Table 2-8 Port Interface

Note: For pins other than those listed above, the R_MTR_InitUnusedPins function in r_mtr_rl78g24.c handles the pins as unused. Please make appropriate changes when changing the terminal arrangement.

2.3.2 Peripheral functions

[Table 2-9](#page-10-0) is a list of peripheral functions used in this system.

Table 2-9 List of Peripheral Functions

Peripheral Function	Usage	
12-bit A/D converter (A/D)	- Inverter bus voltage measurement - U/V/W phase voltages measurement - DC-link current detection	
Timer Array Unit (TAU)	- Free-running timer for rotational speed measurement (TAU1) - Delay timer for changing conducting pattern (TAU3) [Sensorless mode]	
Timer RD2 (TRD2)	- PWM output using extended complementary PWM mode - 50[us] timer	
Timer RG (TRG)	- 1[ms] interval timer	
Timer RJ (TRJ)	- 50[us] timer for ICS communication [Initial Position Detection]	
Timer RX(TRX)	- Current rising period measurement [Initial Position Detection]	
Comparator (CMP3)	- Over current detection - Judgement for reaching threshold current [Initial Position Detection]	
10-bit D/A converter (DA)		
External Interrupt (INTP1, INTP2, INTP3)	- Input signal from Hall effect sensor [Hall effect sensor mode]	
PWM Option Unit A (PWMOPA)	- Forced shut-off of PWM output depending on CMP3 output	
Watch dog timer (WDT)	- Program runaway detection	

(1) 12-bit A/D converter (A/D)

The U phase voltage (Vu), V phase voltage (Vv), W phase voltage (Vw), inverter bus voltage (Vdc), DC link current (Idc) are measuIed by using the '12-bit A/D converter'. [Sensorless mode] Inverter bus voltage (Vdc), DC link current (Idc) are measured by using the '12-bit A/D converter'. [Hall effect sensor control mode] A/D conversion mode is set to the advanced mode and the conversion operation mode to One-shot Conversion mode.

(2) Timer Array Unit (TAU)

a. Free-running timer for rotational speed measurement (TAU1) This channel 1 of TAU is used as free-running counter for rotational speed calculation. b. Delay timer for changing conducting pattern (TAU3) The channel 3 of TAU is used as delay timer for changing conducting pattern with π/6 phase from the zero-crossing point.

(3) Timer RD (TRD)

AD conversion can be executed at any timing using two AD conversion trigger compare registers. Three-phase PWM output of upper arm chopping with dead time (complementary) is performed using the Extended Complementary PWM Mode.

- (4) Timer RG (TRG) Timer RG (TRG) is used as 1[ms] interval timer for speed control.
- (5) Timer RJ (TRJ) Timer RJ (TRJ) is used as timer for ICS communication during initial position detection.
- (6) Timer RX (TRX) Timer RX (TRX) is used as timer for measuring period of reaching threshold current during initial position detection.

- (7) Comparator (CMP3) CMP3 is used for overcurrent or initial position detection. The output of D/A converter is selected for the reference value of CMP3, which is set as the threshold value to be compared with the corresponding current.
- (8) 10-bit D/A Convertor (D/A) The result of D/A converter is used as internal reference value for over current or initial position detection.
- (9) External interrupt (INTP1. INTP2, INTP3) Signals from Hall effect sensors are obtained for detection of rotor position. Both rising and falling edges are selected for detection. When the interruption occurs, input signals from Hall effect sensor are obtained (detection of rotor position), conducting pattern is changed, and calculation of rotational speed is performed.
- (10) PWM Option Unit A (PWMOPA) Force the PWM output to be cut off from the overcurrent signal detected in CMP3. After detecting the cause of the cut-off release, the forced shut-off of the output is released from the software. The output state at the time of interruption is Low-level output.
- (11) Watch Dog Timer (WDT) Watch Dog Timer is used as a runaway detection program.

2.4 Software structure

2.4.1 Software file structure

The folder and file configurations of the sample programs are given below.

Note 1: Regarding the specification of the Analyzer function in the motor control development support tool Renesas Motor Workbench (RMW), please refer to Chapter 4. The identifier ics/ICS (ICS is the previous motor control development support tool, In Circuit Scope) is attached to the names of folders, files, functions, and variables related to Renesas Motor Workbench.

2.4.2 Module configuration

[Figure 2-2](#page-13-0) shows module configuration of the sample programs.

2.5 Software specifications

[Table 2-5](#page-14-0) shows the basic specifications of target software of this application note. For details of 120-degree conducting control, refer to the application note '120-degree conducting control of permanent magnetic synchronous motor: algorithm'.

		2002 \pm 1.1 Bable Opedinoations of Coltinary $1/2$	
Item	Content		
Control method	120-degree conducting method (high-side chopping)		
Motor rotation start/stop	Operation using the motor control development support toolNote		
Position detection of rotor	Hall effect sensor: The positioning of the rotor is obtained based on interruption		
magnetic pole	of signals from Hall effect sensors. (every 60 degrees)		
	Sensorless: The position of the rotor is obtained based on the zero-crossing of		
		the BEMF voltage, which is scaled at the ADC input. (every 60 degrees)	
	- At the change of voltage pattern, PWM duty is updated, and the motor windings		
	are energized accordingly.		
	Initial Position Detection: The position of rotor is estimated using TRX and		
	CMP ₃ .		
	- Angle detection within 180-degree is obtained by using the saliency		
	characteristics of the rotor.		
	- Angle detection within 360-degree is obtained by performing polarity detection		
	using the magnetic saturation characteristics of the rotor.		
Control mode	There are 4 control modes in this sample software.		
		- Sensorless current mode	
		- Sensorless voltage mode	
	- Hall effect sensor-based current mode		
	- Hall effect sensor-based voltage mode		
	For details, please refer to 4.4.		
Input voltage	DC24[V]		
Main clock frequency	CPU clock: f _{CLK} 48[MHz]		
	TRD clock: f _{PLL} 96[MHz]		
Carrier frequency (PWM)	20 [kHz]		
Dead time	1 [μ s]		
Control cycle	Speed PI control: 1 [ms] Current PI control: 50 [µs]		
Range of rotational speed	$CW:0$ [rpm] ~ 3975[rpm]		
control	CCW:0 [rpm] \sim 3975 [rpm]		
		Note that the motor is driven at open-loop mode below 530 [rpm]	
Optimization setting	-Olite		
ROM/RAM Size	ROM	19.512KB [Sensorless current mode]	
		19.008KB [Sensorless voltage mode]	
		15.495KB [Hall effect sensor-based current mode]	
		14.865KB [Hall effect sensor-based voltage mode]	
	RAM	1.130KB [Sensorless current mode]	
		1.078KB [Sensorless voltage mode]	
		0.896KB [Hall effect sensor-based current mode]	
		0.844KB [Hall effect sensor-based voltage mode]	

Table 2-11 Basic Specifications of Software[1/2]

[Note]

1. For details, please refer to "Renesas Motor Workbench"

2. Please refrain from operating the motor for extended period at speed above rated rotational speed.

2.6 User option bytes

The settings of the user option byte area of the RL78/G24 flash memory are shown below.

Setting	Address	Value	Description
783AEA	000C0H /040C0H	01111000B	- Uses watchdog timer interval interrupt: does not use interval interrupt - Period when watchdog timer window is open: 100 [%] - Watchdog timer counter operation control: Counter operation possible (After reset is canceled, count begins) - Watchdog timer overflow time: 100 [ms] - Watchdog timer counter operation control: In HALT/STOP mode, counter operation stops
	000C1H /040C1H	00111010B	- LVD0 off setting
	000C2H /040C2H	11101010B	- Flash operation mode setting: HS (high-speed main) mode - High-speed on-chip oscillator/block frequency fHOCO: 8 [MHz] f.H. 8 [MHz]

Table 2-13 User option byte settings

3. Descriptions of the control program

The target sample programs of this application note are explained here.

3.1 Contents of control

3.1.1 Motor start/stop

The start and stop operations of motor are controlled by inputs from Renesas Motor Workbench.

3.1.2 A/D Converter

(1) Inverter bus voltage

As shown in Table 3-2 below, the inverter bus voltage is measured and used for modulation factor calculation and over-voltage and under-voltage detection. (When an abnormality is detected, PWM is stopped).

(2) U phase, V phase, and W phase voltage

As shown in [Table 3-2](#page-17-1) below, the U, V and W phase voltages are measured and used for determining zerocrossing of BEMF.

Table 3-2 Conversion Ratio of U, V, and W Phase Voltage

(3) DC link shunt resistor current

As shown in [Table 3-3](#page-17-2) below, the DC link shunt resistor current is measured and used for setting threshold current for CMP3.

[Note] For more information about A/D conversion characteristics, see "RL78/G24 User's Manual - Hardware.

3.1.3 Comparator

(1) Overcurrent detection and initial position detection (CMP3)

The output of the A/D is compared with the reference value of the internal D/A converter and used for the overcurrent detection and judgment of the current threshold value for initial position detection.

Figure 3-1 Overcurrent Detection Using CMP3

3.1.4 Voltage control by PWM

PWM control is used for controlling output voltage. The PWM control is a control method that continuously adjusts the average voltage by varying the duty of pulse, as shown in [Figure 3-2](#page-18-0).

Figure 3-2 PWM Control

Here, modulation factor "m" is defined as follows.

$$
m=\frac{V}{E}
$$

 m : Modulation factor V : Command value voltage E : Inverter bus voltage

This modulation factor is set to resisters for PWM duty in TRD.

In the target software of this application note, upper arm chopping is used to control the output voltage and speed. [Figure 3-3](#page-19-0) and [Figure 3-4](#page-19-1) show an example of output waveforms at upper arm chopping. Noncomplementary / complementary PWM can be switched by setting the configuration definition file "r_mtr_config.h".

Figure 3-4 Upper Arm Chopping (Complementary PWM)

3.1.5 State transitions

[Figure 3-5](#page-20-0) shows state transition diagrams of 120-degree conducting control software.

Figure 3-5 State Transition Diagram 120-degree Conducting Control Software

(1) SYSTEM MODE

"SYSTEM MODE" indicates the operating states of the system. "SYSTEM MODE" has 3 states that are motor drive stop (INACTIVE), motor drive (ACTIVE), and abnormal condition (ERROR). (2) RUN MODE

"RUN MODE" indicates the condition of the motor control. The state is changed by occurrence of "EVENT". (3) EVENT

"EVENT" indicates the change of "RUN MODE". When "EVENT" occurs, "RUN MODE" changes as shown table in [Figure 3-5.](#page-20-0) Each "Event" is caused by occurrence as shown in [Table 3-4.](#page-20-1)

"EVENT" name	Occurrence factor	
STOP	By user operation	
DRIVE	By user operation	
ERROR	When the system detects an error	
RESET	By user operation	

Table 3-4 List of "EVENT"

In the DRIVE event of RUN MODE, the DRIVE status changes from the table in [Table 3-5 according to](#page-21-0) [the](#page-21-0) drive status of the motor.

3.1.6 Startup method

(1) Hall effect sensor mode

In the Hall effect sensor mode, after changing to "MTR_MODE_DRIVE", the output pattern is selected from the initial Hall effect sensor signal. Then, voltage is applied, and state is changed to PI control state. The rotational speed is calculated after second hall effect sensor interruption. The start-up sequence for current control mode and voltage control mode is shown in [Figure 3-6](#page-22-0) and [Figure 3-7](#page-22-1) respectively.

Figure 3-6 Start-up sequence for Hall effect sensor-based current control mode

Figure 3-7 Start-up sequence for Hall effect sensor-based voltage control mode

(2) Sensorless mode

In sensorless mode, the position of the magnetic poles is estimated every 60 degrees from induced voltage that is generated from the variation of magnetic flux due to the rotation of the permanent magnet(rotor). However, since the induced voltage is generated by the rotation, at low speed it is not possible to estimate the position of the rotor.

Therefore, the method to generate a rotating magnetic field by forcibly switching conducting pattern in the synchronous speed regardless of the position of rotor, is often used.

[Figure 3-8](#page-23-0) shows the start-up sequence for sensorless current control mode. In "MTR_MODE_DRIVE" the rotor is drawn in. Then, it is driven in open-loop drive and transit to PI control state when the speed of rotation reaches the reference speed to switch to sensorless control.

Figure 3-8 Start-up sequence for sensorless current control mode (Start-up with draw-in)

The start-up sequence for sensorless current control mode using the initial position detection function is shown in [Figure 3-9.](#page-23-1) Instead of using draw-in to align the position of the rotor, initial position detection process is performed, after which open-loop process begins.

Figure 3-9 Start-up sequence for sensorless current control mode, start-up with Initial Position Detection)

[Figure 3-10](#page-24-0) shows the start-up sequence for sensorless voltage control mode. In "MTR_MODE_DRIVE" the rotor is drawn in. Then, it is driven in open-loop drive, and transit smoothly to PI control state after the induced voltage zero crossing signal is detected 3 times.

Figure 3-10 Start-up sequence for sensorless voltage control mode (Start-up with draw-in)

[Figure 3-11](#page-24-1) shows the start-up method for sensorless voltage control mode using initial position detection function.

Figure 3-11 Start-up sequence for sensorless voltage control mode, start-up with Initial Position Detection)

3.1.7 Speed control

In this system, a free-running timer counter is used, and rotational speed is calculated by using the difference between the current timer counter value and the timer counter value 2π [rad] earlier. The counter values are obtained when Hall effect sensor interruption is executed in Hall effect sensor control mode, or when zerocrossing of BEMF voltage is detected in sensorless mode.

Figure 3-12 Method of Calculation for Rotational Speed

3.1.8 Control method

This sample software uses different control systems for current control mode and voltage control mode. In current control mode, the control system is made up of an Auto Speed Regulator (ASR) and an Auto Current Regulator (ACR). In voltage control mode, the control system is only made up of an Auto Speed Regulator (ASR). These controllers are implemented using PI controllers, and the gains are required to be adjusted according to the type of controllers.

3.1.8.1 Control method for current control mode

The block diagram of the entire control system for current control mode is shown in [Figure 3-13.](#page-26-0)

Figure 3-13 Control System Block Diagram (Current control mode)

The speed PI controller and current PI controller are shown as below. The speed PI controller outputs reference current value whereas the current PI controller outputs reference voltage value.

 $i^* = (K_{pASR} + \frac{\kappa_{iASR}}{s})(\omega^* - \omega)$ (1) i^* : Reference current ω^* : Reference rotational speed ω : Rotational speed K_{pASR} : Speed PI proportional gain K_{lASR} : Speed PI integral gain s : Laplace operator $v^* = (K_{pACR} + \frac{\kappa_{iACR}}{s})(i^* - i) \cdot \cdot \cdot (2)$ v^* : Reference voltage i^* : Reference current i : Current K_{pACR} : Current PI proportional gain K_{iACR} : Current PI integral gain s : Laplace operator

3.1.8.2 Control method for voltage control mode

The block diagram of the entire control system for current voltage control mode is shown in [Figure 3-14.](#page-27-0)

Figure 3-14 Control System Block Diagram (Voltage control mode)

The speed PI controller is shown as below. The speed PI controller outputs reference voltage value.

 $v^* = (K_{pASR} + \frac{\kappa_{iASR}}{s})(\omega^* - \omega)$ · · · 3 v^* : Reference voltage ω^* : Reference rotational speed ω : Rotational speed K_{pASR} : Speed PI proportional gain K_{lASR} : Speed PI integral gain s : Laplace operator

3.1.9 Interrupt Processing Specifications

The interrupt processing of this sample software is composed of two cycle interrupts: a carrier cycle interrupt (50[µs]) and a 1-ms cycle interrupt, applicable in both Hall effect sensor mode and sensorless mode. Since the current control system is carried out in the carrier cycle interrupt, the control cycle for the current control system is 50[µs]. On the other hand, since the speed control system is carried out in the 1-ms cycle interrupt, the control cycle for the speed control system is 1[ms].

3.1.9.1 Interrupt processing for current control mode

In current control mode, reference voltage is updated in a 50[µs] interval as the output of current PI controller.

Figure 3-15 Interrupt processing inside control block (open-loop control)

Here is an outline for open-loop drive for current control mode. In open-loop control, only current PI controller is used. Based on the reference voltage obtained as the output of the current PI controller, voltage is applied to the rotor according to the commutation pattern. Each commutation pattern outputs for an electrical angle of 60 degrees, and the commutation patterns are sequentially switched according to the reference speed.

Figure 3-16 Interrupt processing inside control block (sensorless closed loop control)

Figure 3-17 Interrupt processing inside control block (Hall effect sensor-based closed loop control)

Here is an outline for closed loop drive for current control mode. In closed loop control, the rotational speed is calculated based on the rotor position, where it is detected using the zero-crossing detection signal in sensorless mode and Hall effect sensor signal in Hall effect sensor mode. The speed error is input into the speed PI controller and the output is reference current. The current PI controller outputs reference voltage which is then applied to the rotor according to the commutation pattern.

3.1.9.2 Interrupt processing for voltage control mode

In voltage control mode, reference voltage is updated in a 1[ms] interval as the output of speed PI controller.

Figure 3-18 Interrupt processing inside control block (open-loop control)

Here is an outline for open-loop drive for voltage control mode. In open-loop control, speed PI controller is not used. Therefore, constant voltage is applied to the rotor according to the commutation pattern. Each commutation pattern outputs for an electrical angle of 60 degrees, and the commutation patterns are sequentially switched according to the reference speed.

Figure 3-20 Interrupt processing inside control block (Hall effect sensor-based closed loop control)

Here is an outline for closed loop drive for voltage control mode. In closed loop control, the rotational speed is calculated based on the rotor position, where it is detected using the zero-crossing detection signal in sensorless mode and Hall effect sensor signal in Hall effect sensor mode. The speed error is input into the speed PI controller and the output is reference voltage, which is then applied to the rotor according to the commutation pattern.

3.1.10 DC link current, bus voltage and phase voltage measurement method

This section explains the method used in this sample program to measure DC link current, bus voltage and phase voltage

3.1.10.1 Timing to measure DC link current, bus voltage and phase voltage

In this sample program, the following functions of RL78/G24 is used to measure DC link current, bus voltage and phase voltage.

- Timer RD2

Extended complementary PWM mode and A/D conversion trigger 0,1

- A/D converter

Advanced mode and hardware trigger mode

In this sample program, DC link current, bus voltage and phase voltage are measured over two carrier cycles. [Figure 3-21](#page-31-0) shows an example of extended complementary PWM waveforms.

Figure 3-21 Extended complementary PWM waveforms (Example: U phase: upper arm ON. V phase: lower arm ON, W phase: non-energized phase)

In the first carrier cycle, the DC link current and the non-energized phase voltage (W phase) are measured at point A i[n Figure 3-21.](#page-31-0) At point B, the non-energized phase voltage (W phase) and the phase voltage where the upper arm is turned on (U phase) are measured. In the second carrier cycle, the bus voltage and the non-energized phase voltage (W phase) are measured at point C. At point D, the non-energized phase voltage (W phase) and the phase voltage where the upper arm that is turned on (U phase) are measured. By shifting the position of the A/D conversion trigger closer to the peak of the carrier in the second cycle, nonenergized phase voltage measurements are taken at four different points. The average of the measurement result is used as the non-energized phase voltage for control.

3.1.10.2 A/D conversion trigger timing adjustment

In this sample program, the induced voltage of the non-energized phase voltage is measured when the upper arm of the PWM is turned on. The induced voltage waveform typically appears as a damped oscillation after the upper arm is turned on. Since the measurement values vary depending on the A/D conversion trigger timing, the appropriate induced voltage is measured as follow. Two A/D conversion are performed within the period where the upper arm is turned on, and the average of the values over two carrier cycles is used. Therefore, it is necessary to adjust the A/D conversion trigger timing according to the duty value.

A threshold for duty value is set, and the A/D conversion trigger timing is switched based on whether the duty value is above or below the threshold. This prevents the A/D conversion process from overlapping with the timing of valley of carrier cycle where the setting of trigger is set. The threshold for the duty value is a tunable parameter.

When the duty value is below the threshold, A/D conversion trigger is set as shown in [Figure 3-22.](#page-32-0) The A/D conversion trigger timing (1) from the ON/OFF edge of the upper arm, and the interval (2)) between the A/D conversion trigger in first and second carrier are tunable parameters.

When the duty value exceeds the threshold, A/D conversion trigger 1 is fixed at the trigger position for the minimum duty value, as shown in [Figure 3-23.](#page-32-1)

Figure 3-22 A/D conversion timing (Duty value is below threshold)

Figure 3-23 A/D conversion timing (Duty exceeds threshold value)

The following [Table 3-6](#page-33-0) shows the parameters and variables corresponding to the duty value threshold, the A/D conversion trigger timing (1) from the ON/OFF edge of the upper arm, and the interval (2) between the A/D conversion trigger in first and second carrier as shown in [Figure 3-22](#page-32-0) and [Figure 3-23.](#page-32-1)

3.1.11 Initial position detection of a stationary rotor using saliency characteristic

A motor is said to have saliency if the magnetic resistance varies according to the position of the rotor. If the magnetic resistance changes sinusoidally, then the inductance will also change sinusoidally. As shown in [Figure 3-24,](#page-34-0) inductance changes at twice the period of the rotor. In this case, when voltage is applied so that current flows from U→V, V→W, and W→U, the time it takes for the current flowing through the shunt to reach the threshold current value changes according to the position of the rotor. An example of this is shown in [Figure 3-25.](#page-34-1) It therefore takes longer when voltage is applied in the V→W direction than when voltage is applied in the W→U direction.

Figure 3-24 Changes in inductance according to the position of the rotor

Figure 3-25 Relationship between rotor position and each phase

Here is a description of the rotor position detection method using this phenomenon. A diagram of the angle detection for salient motor used in this system is shown in [Figure 3-26.](#page-35-0) It is distinguished by applying 3 patterns of voltage, measuring the time taken for the current that flows through the shunt resistor to reach the threshold current, and comparing these to detect the direction of the rotor facing in every 60 degrees within the 180 degrees of electrical angle.

Figure 3-26 Angle detection diagram

The algorithm used in this system detects the time taken to reach the Internal reference current value using an RL78/G24 timer RX (TRX) and a comparator 3 (CMP3). It uses the TRD2 extended complementary PWM mode to apply pulse-shaped voltage to each phase. The count of the TRX starts at the rising edge synchronization of the TRD. The CMP3 generates an interrupt when it detects that the current flowing through the shunt resistor has reached the threshold current, and the current rise time required is measured.

Angle detection by saliency is performed every 60 degrees within the 180 degrees of electrical angle by comparing the cumulative time measured at each phase. Measurement ends when the cumulative time difference between the maximum phase and the minimum phase is greater than or equals to the threshold value. However, if the difference does not reach the threshold after the maximum number of measurements, angle detection by saliency is judged as failure.

Figure 3-27 Current detection time differential among the 3-Phases

To confirm that the motor rotor has sufficient saliency to estimate its initial position, saliency judgement is performed. TRX count increases with the current rise during the measurement for 3-phases. The difference

between maximum value and median value of the TRX count, and the difference between median value and minimum value of the TRX count, is compared and the phase with maximum difference is identified as the phase with maximum value or the phase with minimum value. Next, it applies voltage in the direction opposite to the identified phase and measures the time required for the current to rise. In this case, the mean value of the TRX count for the 2-phases is compared to the TRX count for the phase with the energization direction reversed. If the TRX count of the reversed phase has the same magnitude relation with the identified phase, saliency is judged to be sufficient, and if it does not, saliency is judged to be too low.

For example, as shown in [Figure 3-28](#page-36-0) if the rotor is oriented in the 120-degree direction, the phase identified will be the W-U phase because the difference between the maximum value and the median value is greater. By reversing the energization direction from the W-U phase, voltage is applied to the U-W phase, and the time take for current rise is measured. Compare the median value of the TRX counts of the U-V, V-W, and W-U phase, with the TRX count of U-W phase. If the U-W phase TRX count is greater, initial position detection using saliency is judged to be possible, but if it is lower, it is judged not to be possible.

Figure 3-28 Saliency confirmation method

3.1.12 Initial position detection by saturation

Since the method described above uses the change in inductance due to saliency to estimate the position, it is not possible to determine the polarity (for example, there is no distinction between 60 degrees and 240 degrees). Also, it cannot be applied when a non-salient motor is used. Here, the magnetic saturation characteristics of the motor are used for polarity detection and angle detection with a non-salient rotor.

Due to the limited amount of magnetization that a magnetic material can have, if current is applied to a coil to generate an external magnetic field around the core of the coil, the core goes into a state of saturated magnetization when the external magnetic field exceeds a certain value. If the direction of the external magnetic field through the core is the same as the orientation of the magnetic field generated by the current flowing into the coil, the inductance becomes smaller because magnetization is more saturated than if the directions were opposite. These characteristics are used to judge the orientation of the magnetic pole.

Figure 3-29 Example of magnetic pole wound with coil

Figure 3-30 Current differential according to direction of applied current

Voltage is applied to the motor as shown in [Figure 3-30](#page-37-0) and the time required for the current flowing in the shunt resistor to rise is measured by TRX in the same way as it is measured when using saliency. For measurements using saturation characteristics, the TRX count is lowest when the direction of the voltage applied matches the direction of rotation, so this tendency is used to estimate the orientation of the rotor.

In the case of salient motor, to detect polarity by saturation, voltage is applied forward and backward based on the result of angle detection by saliency. The polarity of the rotor is determined by comparing the magnitude relation of current rise time. In the case of non-salient motor, the current rise time is measured by applying voltage in 6 directions, and the angle detection by saturation is performed by assuming the rotor is facing the phase with the minimum TRX count value.

Figure 3-31 Example of applied voltage pattern due to initial position detection using magnetic saturation

Measurement stops when the TRX count difference for each directions exceed the threshold value. However, when the cumulative value of the TRX count difference does not reach the threshold value even after the maximum number of measurements, initial position detection is judged as success if the cumulative value is above the percentage of threshold set, whereas initial position detection is judged as failure if the cumulative value is less than percentage of threshold set.

The initial position detection process to be performed changes depending on the value of the preparation method for start-up (PS_METHOD). [Table 3-7](#page-38-0) shows the processes executed in each mode.

3.1.13 Advanced angle control

As the rotational speed increases, the phase of the current tends to lag the induced voltage of each phase voltage. When this phase lag occurs, the torque cannot be increased. Therefore, a method called advanced angle control is used, which the phase of the applied voltage is advanced such that the phase of the induced voltage and current coincide. In this sample program, by decreasing the angle delayed between BEMF zerocrossing detection and step commutation, angle can be advanced up to 30 degrees. In order to advance angle above 30 degrees, it is achieved by adjusting the value of the comparison voltage for BEMF zero-crossing detection (the midpoint voltage used for comparison with each phase's induced voltage).

3.1.14 System protection function

This program has the following types of error states, and executes an emergency stop function in the event that any of the following errors occur. Refer to [Table 3-8](#page-40-0) for the settings of the system protection functions.

- Hardware overcurrent error

When the CMP3 interruption (overcurrent detection) is generated, voltage output is stopped.

- Software overcurrent error

3-phase current are monitored in the overvoltage monitoring cycle. When overvoltage (value exceeding the overvoltage limit) is detected, an emergency stop occurs.

- Overvoltage error

The inverter bus voltage is monitored in the overvoltage monitoring cycle. When overvoltage (value exceeding the overvoltage limit) is detected, an emergency stop occurs. The overvoltage limit is set in consideration of the error of the resistance value of the detection circuit.

- Undervoltage error

The inverter bus voltage is monitored in the undervoltage monitoring cycle. When undervoltage is detected (when it goes below the undervoltage limit), an emergency stop occurs. The undervoltage limit is set in consideration of the error of the resistance value of the detection circuit.

- Rotational speed error

The speed is monitored in the rotational speed monitoring cycle. When the speed limit value is exceeded, an emergency stop occurs.

- Timeout error

The timeout counter is monitored at the timeout monitoring cycle. When pattern switching by Hall effect sensor interruption in Hall effect sensor control mode or zero-crossing of induced voltage in sensorless control mode don't happen for a timeout period, voltage output is stopped.

- Pattern error

The output voltage pattern is monitored at the pattern monitoring cycle. When unexpected pattern is detected in voltage pattern set from Hall effect sensor in Hall effect sensor control mode or induced voltage in sensorless control mode, voltage output is stopped.

- TRX overflow error

When TRX counter overflows at measuring period of current rising in initial position detection process, voltage output is stopped.

Table 3-8 System Protection Function Settings

3.1.15 PU system

The dynamic range of motor control is determined during compiling using fixed point arithmetic. If there is a large difference between the actual motor characteristic and the hypothetical motor characteristic during design, problems such as overflow and rounding errors tend to occur due to differences in dynamic ranges. The program uses the per-unit method (PU: per-unit) in order to reduce the calculated dynamic range's dependency on the motor characteristics. The PU value of any physical quantity is its value relative to a base physical quantity, and can be derived as follows:

PU Value = $\frac{Physical\ quantit}{Base\ Value}$

All PU units used for control, such as physical quantity and gain, can be derived from the base current, base voltage, base frequency, and base angle. For example, base resistance can be calculated from the base voltage and base current:

⁼

The effect of motor characteristics on calculated dynamic range is reduced, so it is necessary to set standard values for current, voltage, and angular frequency based on the motor characteristics (the method of deriving the standard value is not unique). In this program, rated current, voltage input to inverter, and maximum speed are set to standard values (PU units) for current, voltage, and angular frequency. The base value for each physical quantity is shown in [Table 3-9.](#page-41-0) These values are defined in r_mtr_scaling_parameter.h.

Table 3-9 PU system base values

3.2 Function specifications of 120-degree conducting control software

Lists of functions used in this control program are shown below. Functions not used in this system are not listed.

Table 3-11 List of Functions "r_mtr_ics.c"

Table 3-12 List of Functions "r_mtr_board.c"

Table 3-13 List of Functions "ICS2_RL78G24.lib"

Table 3-14 List of Functions "R_DSP_RL78_CC_S.lib"

Table 3-15 List of Functions "r_mtr_driver_access.c"

Table 3-16 List of Functions "r_mtr_statemachine.c"

Table 3-17 List of Functions "r_mtr_120.c"

Table 3-18 List of Functions "r_mtr_ctrl_gain_calc.obj"

Table 3-19 List of Functions "r_mtr_interrupt.c" [1/3]

Table 3-20 List of Functions "r_mtr_interrupt.c" [2/3]

Table 3-22 List of Functions "r_mtr_ipd.h"

Table 3-23 List of Functions "r_mtr_ipd.c"

Table 3-1 List of Functions "r_mtr_ol2cl_ctrl.c"

Table 3-25 List of Functions "r_mtr_aa_ctrl.obj"

Table 3-26 List of Functions "r_mtr_rl78g24.c"

Table 3-27 List of Functions "Config_COMP3_user.c"

Table 3-28 List of Functions "Config_TRG.h"

Table 3-29 List of Functions "Config_TAU0_3_user.h"

Table 3-31 List of Functions "Config_PWMOPA_user.c"

Table 3-32 List of Functions "Config_TRD0_TRD1.h"

Table 3-33 List of Functions "Config_TRD0_TRD1.c"

Table 3-34 List of Functions "Config_ADC_user.c"

3.3 Lists of variables of sensorless 120-degree conducting control software

Lists of variables used in this control program are shown below. However, note that the local variables are not mentioned.

In the sample programs, fixed-point number is used for calculation. Therefore, in advance, some control variables are set in fixed-point number. Bits number in fractional part of fixed-point number is expressed in the Q format. "Qn" means n bits left shift.

Table 3-36 List of variables "r_mtr_ics.c"[1/2]

Table 3-37 List of variables "r_mtr_ics.c"[2/2]

Table 3-38 List of variables "r_mtr_parameter.h / Structure : st_mtr_parameter_t"

Table 3-39 List of variables "r_mtr_driver_access.h / Structure : mtr_ctrl_input_t"[1/2]

Table 3-42 List of variables "r_mtr_statemachine.h / Structure : st_mtr_statemachine_t"

Table 3-43 List of variables "r_mtr_statemachine.c"

Table 3-44 List of variables "r_mtr_120.h / Structure : st_mtr_v_pi_t"

Table 3-45 List of variables "r_mtr_120.h / Structure : st_mtr_pi_t"

Table 3-46 List of variables "r_mtr_120.h / Structure : st_mtr_acr_t"

Table 3-47 List of variables "r_mtr_120.h / Structure : st_mtr_asr_t"

Table 3-48 List of variables "r_mtr_120.h / Structure : st_mtr_hall_control_t"

Table 3-49 List of variables "r_mtr_120.h / Structure : st_mtr_sensorless_control_t"[1/2]

Table 3-50 List of variables "r_mtr_120.h / Structure : st_mtr_sensorless_control_t"[2/2]

Table 3-51 List of variables "r_mtr_120.h / Structure : st_mtr_120_control_t" [1/2]

Table 3-52 List of variables "r_mtr_120.h / Structure : st_mtr_120_control_t" [1/2]

Table 3-53 List of variables "r_mtr_120.c"

Table 3-54 List of variables "r_mtr_interrupt.c"

Table 3-55 List of variables "r_mtr_ctrl_gain.h / Structure : st_mtr_ctrl_gain_voltage_mode_t"

Table 3-56 List of variables "r_mtr_ctrl_gain.h / Structure : st_mtr_ctrl_gain_current_mode_t"

Table 3-57 List of variables "r_mtr_ctrl_gain.h / Structure : st_design_parameter_t"

Table 3-58 List of variables "r_mtr_ipd.h / Structure : st_mtr_ipd_t"

Table 3-59 List of variables "r_mtr_120.h / Structure : st_mtr_ol2cl_t"

Table 3-60 List of variables "r_mtr_aa_ctrl.h / Structure : st_mtr_aa_pi_t"

Table 3-61 List of variables "r_mtr_aa_ctrl.h / Structure : st_mtr_aa_lpf1_t"

Table 3-62 List of variables "r_mtr_aa_ctrl.h / Structure : st_mtr_aa_t"

3.4 Macro definitions of sensorless 120-degree conducting control software

Lists of macro definitions used in this control program are shown below.

Table 3-64 List of Macro definitions "r_mtr_motor_parameter.h"

Table 3-65 List of Macro definitions "r_mtr_inverter_parameter.h"

Table 3-66 List of Macro definitions "r_mtr_control_parameter.h"[1/2]

Table 3-67 List of Macro definitions "r_mtr_control_parameter.h"[2/2]

Table 3-68 List of Macro definitions "r_mtr_scaling_parameter.h"[1/2]

Table 3-69 List of Macro definitions "r_mtr_scaling_parameter.h"[2/2]

Table 3-70 List of Macro definitions "main.h"

Table 3-71 List of Macro definitions "ICS_define.h"

Table 3-72 List of Macro definitions "r_mtr_ics.h"

Table 3-73 List of Macro definitions "r_mtr_ctrl_rl78g24.h"[1/2]

Table 3-74 List of Macro definitions "r_mtr_ctrl_rl78g24.h"[2/2]

Table 3-75 List of Macro definitions "r_mtr_common.h"

Table 3-76 List of Macro definitions "r_mtr_parameter.h"

Macro	Definition value	Qn	PU	Description	Remarks
MTR SPEED PI LIMIT V	IP INPUT V			Output voltage limit at PI control	
MTR MCU ON V	IP INPUT V * 0.8f	$\frac{1}{2}$	$\overline{}$	MCU stable supply voltage	
MTR US MAX DRIVE V	IP INPUT V * 0.96f	$\frac{1}{2}$	$\overline{}$	Maximum output voltage	
MTR US MIN DRIVE V	IP INPUT V * 0.0f	\overline{a}	\sim	Minimum output voltage	
MTR MAX DRIVE V	FIX fromfloat(MTR US MAX DRIVE V* PU SF VOLTAGE, MTR_Q_VOLTAGE)	Q13	Voltag e	Maximum output voltage	
MTR MIN DRIVE V	FIX fromfloat(MTR US MIN DRIVE V* PU_SF_VOLTAGE, MTR_Q_VOLTAGE)	Q13	Voltag e	Minimum output voltage	
MTR US SPEED CALC BA SE	MTR TAU1_TIMER_FR EQ* 1000 *MTR TWOPI	\blacksquare	\blacksquare	Calculation parameter to convert the timer counter to rotational speed	
MTR_SPEED_CALC_BASE	FIX32 fromfloat(MTR U S SPEED CALC BASE * PU_SF_AFREQ, MTR Q AFREQ)	Q ₁₄	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed	
MTR_OL_SPEED_CALC_BAS E.	MTR CARRIER FREQ * 1000 * MTR_TWOPI / MTR_PATTERN_NUM	\blacksquare	$\mathcal{L}^{\mathcal{A}}$	Calculation parameter to convert rotational speed to timer counter at open-loop drive	
MTR PU Q OL SPEED CAL C BASE	FIX32 fromfloat(MTR U S OL SPEED CALC B ASE * PU_SF_AFREQ,MTR_Q AFREQ)	Q14	Angul ar freque ncy	Calculation parameter to convert rotational speed to timer counter at open-loop drive	
MTR ASR DEADBAND	Ω	\overline{a}	\blacksquare	Minimum value of deadband for integral term	
MTR_SPEED_CALC_BASE_1 ST	MTR_SPEED_CALC_B ASE/6	Q14	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed at first speed calculation	
MTR_SPEED_CALC_BASE_2 ND.	MTR SPEED CALC B ASE/3	Q ₁₄	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed at second speed calculation	
MTR_SPEED_CALC_BASE_3 RD	MTR SPEED CALC B ASE/2	Q ₁₄	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed at third speed calculation	
MTR_SPEED_CALC_BASE_4 TH	MTR SPEED CALC B ASE*2/3	Q ₁₄	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed at fourth speed calculation	
MTR SPEED CALC BASE 5 TH	MTR SPEED CALC B ASE*5/6	Q14	Angul ar freque ncy	Calculation parameter to convert the timer counter to rotational speed at fifth speed calculation	
MTR_BIT_SFT_NUM_FOR_D UTY_CALC	15	$\qquad \qquad \blacksquare$		Number of bits shift for duty calculation	
MTR_BIT_SFT_FOR_DUTY_ CALC	(((uint32 t)(1)) << MTR BIT SFT NUM F OR DUTY CALC)	$\qquad \qquad \blacksquare$	$\overline{}$	Bits shifted to the left to improve accuracy of diuty calculation	
MTR_LIMIT_IDC	MP RATED CURRENT * MTR SQRT 3	Q13	Curren t	Speed PI output limit value	[Current control
MTR_I_LIMIT_CURRENT	MP RATED CURRENT * MTR SQRT 3	Q13	Curren	Limit value for speed PI integral term output	mode]
MTR I LIMIT VQ	IP_INPUT_V * 0.9f	Q13	Curren	Current PI Integral term limit	
MTR_MIN_IDC_REF	0	Q13	Curren t	Minimum value for reference current	

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Table 3-77 List of Macro definitions "r_mtr_statemachine.h"

Table 3-78 List of Macro definitions "r_ol2cl_ctrl.h"

Table 3-79 List of Macro definitions "r_mtr_aa_ctrl.h"

Table 3-80 List of Macro definitions "r_mtr_120.h"[1/2]

Table 3-81 List of Macro definitions "r_mtr_120.h"[2/2]

Table 3-83 List of Macro definitions "r_mtr_ipd.h"[2/2]

Table 3-84 List of Macro definitions "Config_TAU0_1.h"

Table 3-85 List of Macro definitions "Config_INTC.h"

Table 3-86 List of Macro definitions "Config_INTC.h"

Table 3-87 List of Macro definitions "Config_TRD0_TRD1.h"

Table 3-88 List of Macro definitions "Config_ADC.h"

3.5 Control flows (flow charts)

3.5.1 Main process

Figure 3-32 Main Process Flowchart

3.5.3 Carrier cycle interrupt handling (Sensorless mode)

Figure 3-33 Carrier Cycle Interrupt Handling (Sensorless mode)

3.5.4 1 [ms] interrupt handling (Sensorless mode)

Figure 3-34 1 [ms] Interrupt Handling (Sensorless mode)

Figure 3-35 Over Current Detection Interrupt Handling

3.5.6 Delay timer interrupt handling

Figure 3-36 Delay Timer Interrupt Handling

3.5.7 Carrier cycle interrupt handling (Hall effect sensor mode)

Figure 3-37 Carrier Cycle Interrupt Handling (Hall effect sensor mode)

3.5.8 1 [ms] interrupt handling (Hall effect sensor mode)

3.5.9 Hall effect sensor interrupt handling

Figure 3-39 Hall effect sensor Interrupt Handling

4. Usage of Motor Control Development Support Tool, 'Renesas Motor Workbench'

4.1 Overview

In the target sample programs described in this application note, you can use user interfaces (rotation/stop command, rotational speed command, etc.) based on the motor control development support tool Renesas Motor Workbench. Please refer to the 'Renesas Motor Workbench User's Manual' for usage and more details. You can find the 'Renesas Motor Workbench' on Renesas Electronics Corporation's website.

Figure 4-1 Renesas Motor Workbench– Appearance

How to use the motor control development support tool, Renesas Motor Workbench

- (1) Start Renesas Motor Workbench by clicking this icon **Renesas Moto**
(2) From the manual work of the motor .
- (2) From the menu bar in the main window, select [File] -> [Open RMT File(O)]. Select RMT file in '[Project Folder]/application/ics/'.
- (3) Use the 'Connection' COM select menu to choose the COM port.
- (4) Click the 'Analyzer' icon on the right side of the Main Window. (The Analyzer Window will be displayed.)
- (5) Please refer to ['4.3](#page-95-0) [Operation Example for Analyzer'](#page-95-0) for the motor driving operation.

4.2 List of variables for Analyzer

[Table 4-1](#page-93-0) and [Table 4-2](#page-94-0) show the list of variables for the Analyzer. These variable values are reflected to the protect variables when the same values as g_s2_enable_write are written to com_s2_enable_write. However, note that variables with (*) do not depend on com_s2_enable_write.

Table 4-1 List of Variables for Analyzer [1/2]

Table 4-2 List of Variables for Analyzer [2/2]

4.3 Operation Example for Analyzer

An example of a motor driving operation using Analyzer is shown below. For the operation, the "Control Window" shown in "Renesas Motor Workbench" is used. Refer to the 'Renesas Motor Workbench V 3.1.2 User's Manual' for details about the "Control Window."

- Driving the motor
- ① Confirm that the [W?] check boxes contain checkmarks for "com_u1_run_event", "com_s2_ref_speed_rpm", and "com_s2_enable_write."
- ② Input a reference rotational speed value in the [Write] box of "com_s2_ref_speed_rpm."
- ③ Click the "Write" button.
- ④ Click the "Read" button. Confirm the [Read] box of "com_s2_ref_speed_rpm" and "g_s2_enable_write."
- ⑤ Input the value in the [Read] box of "g_s2_enable_write", confirmed in step (4), in the [Write] box of "com_s2_enable_write."
- ⑥ Input a value of "1" in the [Write] box of "com_u1_run_event."
- ⑦ Click the "Write" button.

Figure 4-2 Procedure - Driving the motor

Stop the motor

- ① Input a value of "0" in the [Write] box of "com_u1_run_event."
- ② Click the "Write" button.

Figure 4-3 Procedure - Stop the motor

- Error cancel operation
- ① Input a value of "3" in the [Write] box of "com_u1_run_event."
- ② Click the "Write" button.

Figure 4-4 Procedure - Error cancel operation

4.4 Method to switch between control modes

In this sample software, there are four control modes provided. By changing the definition value of "MTRCONF_MODE" in the "r_mtr_config.h" file, you can switch between the four control modes as shown in the following table.

סטטווו שטווווווט וסי וושטוווויס אוסי					
Macro	Content	Remarks			
SENSORLESS CURRENT	Sensorless current mode	Default setting			
SENSORLESS VOLTAGAE	Sensorless voltage mode				
HALL CURRENT	Hall effect sensor-based current mode				
HALL VOLTAGE	Hall effect sensor-based voltage mode				

Table 4-3 Definition of control mode

You can program the device to operate in the specified control mode by changing the definition value and recompiling in the IDE.

Revision History

General Precautions in the Handling of Microprocessing Unit and Microcontroller Unit Products

The following usage notes are applicable to all Microprocessing unit and Microcontroller unit products from Renesas. For detailed usage notes on the products covered by this document, refer to the relevant sections of the document as well as any technical updates that have been issued for the products. 1. Precaution against Electrostatic Discharge (ESD)

A strong electrical field, when exposed to a CMOS device, can cause destruction of the gate oxide and ultimately degrade the device operation. Steps must be taken to stop the generation of static electricity as much as possible, and quickly dissipate it when it occurs. Environmental control must be adequate. When it is dry, a humidifier should be used. This is recommended to avoid using insulators that can easily build up static electricity. Semiconductor devices must be stored and transported in an anti-static container, static shielding bag or conductive material. All test and measurement tools including work benches and floors must be grounded. The operator must also be grounded using a wrist strap. Semiconductor devices must not be touched with bare hands. Similar precautions must be taken for printed circuit boards with mounted semiconductor devices. 2. Processing at power-on

The state of the product is undefined at the time when power is supplied. The states of internal circuits in the LSI are indeterminate and the states of register settings and pins are undefined at the time when power is supplied. In a finished product where the reset signal is applied to the external reset pin, the states of pins are not guaranteed from the time when power is supplied until the reset process is completed. In a similar way, the states of pins in a product that is reset by an on-chip power-on reset function are not guaranteed from the time when power is supplied until the power reaches the level at which resetting is specified.

3. Input of signal during power-off state

Do not input signals or an I/O pull-up power supply while the device is powered off. The current injection that results from input of such a signal or I/O pull-up power supply may cause malfunction and the abnormal current that passes in the device at this time may cause degradation of internal elements. Follow the guideline for input signal during power-off state as described in your product documentation.

4. Handling of unused pins

Handle unused pins in accordance with the directions given under handling of unused pins in the manual. The input pins of CMOS products are generally in the high-impedance state. In operation with an unused pin in the open-circuit state, extra electromagnetic noise is induced in the vicinity of the LSI, an associated shoot-through current flows internally, and malfunctions occur due to the false recognition of the pin state as an input signal become possible.

5. Clock signals

After applying a reset, only release the reset line after the operating clock signal becomes stable. When switching the clock signal during program execution, wait until the target clock signal is stabilized. When the clock signal is generated with an external resonator or from an external oscillator during a reset, ensure that the reset line is only released after full stabilization of the clock signal. Additionally, when switching to a clock signal produced with an external resonator or by an external oscillator while program execution is in progress, wait until the target clock signal is stable.

6. Voltage application waveform at input pin

Waveform distortion due to input noise or a reflected wave may cause malfunction. If the input of the CMOS device stays in the area between V_{IL} (Max.) and V_{IH} (Min.) due to noise, for example, the device may malfunction. Take care to prevent chattering noise from entering the device when the input level is fixed, and also in the transition period when the input level passes through the area between V_{II} (Max.) and V_{II} (Min.).

7. Prohibition of access to reserved addresses

Access to reserved addresses is prohibited. The reserved addresses are provided for possible future expansion of functions. Do not access these addresses as the correct operation of the LSI is not guaranteed.

8. Differences between products

Before changing from one product to another, for example to a product with a different part number, confirm that the change will not lead to problems. The characteristics of a microprocessing unit or microcontroller unit products in the same group but having a different part number might differ in terms of internal memory capacity, layout pattern, and other factors, which can affect the ranges of electrical characteristics, such as characteristic values, operating margins, immunity to noise, and amount of radiated noise. When changing to a product with a different part number, implement a systemevaluation test for the given product.

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