# **DATA SHEET**

# **General Description**

The IDT8V44N003I is a programmable LVDS synthesizer designed for applications requiring frequency conversion from a differential or single-end reference source. The device is designed to provide optimum performance of low phase noise and high power supply noise rejection over a wide range of output frequencies. Oscillator level phase noise performance is achieved through the use of IDT's Fourth Generation FemtoClock®NG PLL technology. Default output frequency settings are factory programmable via a one time programmable ROM while the  $1^2C$  interface can be used to program the output frequency after power up. A buffered copy of the input reference clock is provided at both LVDS output levels for applications requiring efficient board space utilization.

### **Features**

- **•** Fourth generation FemtoClock® (NG) technology
- **•** Reference clock input accepts differential HCSL, LVDS, LVPECL or single-ended sine wave or LVCMOS input levels
- **•** Input frequency range of 20MHz to 500MHz
- **•** Output frequency range of 50MHz to 1.2GHz
- **•** Buffered copy of input reference clock at LVDS output levels
- **•** PLL lock indicator
- **•** Full 3.3V output supply mode
- **•** -40°C to 85°C ambient operating temperature
- **•** Available in lead-free (RoHS 6) package

### **Pin Assignment**



Top View

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# **Block Diagram**



# **Table 1. Pin Descriptions**



NOTE: *Pullup and Pulldown* refer to internal input resistors. See Table 2, *Pin Characteristics,* for typical values.

### **Table 2. Pin Characteristics**



## **Block Diagram with Programming Registers**



# **Register Settings**

# **Table 3A. I2C Register Map**



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# **Table 3B. I2C Register Function Descriptions**



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#### **Table 3C. Input Divider P Coding**



#### **Table 3D. PLL Post Divider N Coding**



NOTE: "X" can be either 0 or 1 (don't care).

### **Serial Interface Configuration Description**

The IDT8V44003I has an I<sup>2</sup>C-compatible configuration interface to access any of the internal registers (Table 3A) for frequency and PLL parameter programming. The IDT8V44003I acts as a slave device on the I2C bus and has the address 0b1101110. The interface accepts byte-oriented block write and block read operations. An address byte (P) specifies the register address (Table 3A) as the byte position of the first register to write or read. Data bytes (registers) are accessed in sequential order from the lowest to the highest byte (most

significant bit first, see Tables 3F, 3G). Read and write block transfers can be stopped after any complete byte transfer. It is recommended to terminate the I<sup>2</sup>C read or write transfer after accessing byte #23 by sending a stop command.

For full electrical I<sup>2</sup>C compliance, it is recommended to use external pull-up resistors for SDATA and SCLK. The internal pull-up resistors have a size of 51kΩ typical.

#### **Table 3E. I2C Device Slave Address**



#### **Table 3F. Block Write Operation**



#### **Table 3G. Block Read Operation**



#### **Table 3H. Default Frequency Settings**



NOTE: Output frequency based on REF\_CLKIN = 80MHz

### **Absolute Maximum Ratings**

NOTE: Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These ratings are stress specifications only. Functional operation of product at these conditions or any conditions beyond those listed in the *DC Characteristics or AC Characteristics* is not implied. Exposure to absolute maximum rating conditions for extended periods may affect product reliability.



NOTE 1: According to JEDEC/JESD 22-A114/22-C101.

### **DC Electrical Characteristics**

**Table 4A. Power Supply DC Characteristics,**  $V_{DD} = 3.3V \pm 5\%$ ,  $T_A = -40^{\circ}C$  to 85°C



#### **Table 4B. LVCMOS/LVTTL DC Characteristics,**  $V_{DD} = 3.3V \pm 5\%$ ,  $T_A = -40^{\circ}C$  to 85°C





#### **Table 4C. Differential DC Characteristics,**  $V_{DD} = 3.3V \pm 5\%$ ,  $T_A = -40\degree C$  to  $85\degree C$

NOTE 1. Common mode voltage is defined as the crosspoint.

# **Table 4D. LVDS DC Characteristics,**  $V_{DD} = 3.3V \pm 5\%$ ,  $T_A = -40\degree C$  to 85 $\degree C$



## **AC Electrical Characteristics**



**Table 5. AC Characteristics,**  $V_{DD} = 3.3V \pm 5\%$ ,  $T_A = -40^{\circ}C$  to  $85^{\circ}C$ 





NOTE: Electrical parameters are guaranteed over the specified ambient operating temperature range, which is established when the device is mounted in a test socket with maintained transverse airflow greater than 500 lfpm. The device will meet specifications after thermal equilibrium has been reached under these conditions.

NOTE 1: Measured from the differential input crossing point to the differential output crossing point.

NOTE 2: Q, nQ outputs measured differentially. See *Output Isolation diagram* in the *Parameter Measurement Information section.*

NOTE 3. Measured using a Rohde & Schwarz SMA100 signal generator, 9kHz to 6GHz as the input source with ±500mV sinewave single-ended input to REF\_CLKIN.

### **Single Side Band Noise Power (80MHz)**



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### **RMS Phase Jitter (480MHz)**

### **Additive Phase Jitter**

The spectral purity in a band at a specific offset from the fundamental compared to the power of the fundamental is called the *dBc Phase Noise.* This value is normally expressed using a Phase noise plot and is most often the specified plot in many applications. Phase noise is defined as the ratio of the noise power present in a 1Hz band at a specified offset from the fundamental frequency to the power value of the fundamental. This ratio is expressed in decibels (dBm) or a ratio

of the power in the 1Hz band to the power in the fundamental. When the required offset is specified, the phase noise is called a *dBc* value, which simply means dBm at a specified offset from the fundamental. By investigating jitter in the frequency domain, we get a better understanding of its effects on the desired application over the entire time record of the signal. It is mathematically possible to calculate an expected bit error rate given a phase noise plot.



**Offset from Carrier Frequency (Hz)**

Measured using a Rohde & Schwarz SMA100 as the input source.

As with most timing specifications, phase noise measurements has issues relating to the limitations of the equipment. Often the noise floor of the equipment is higher than the noise floor of the device. This is illustrated above. The device meets the noise floor of what is shown, but can actually be lower. The phase noise is dependent on the input source and measurement equipment.

### **Parameter Measurement Information**



**3.3V LVDS Output Load AC Test Circuit**



**Propagation Delay**



**Output Isolation (**Q, nQ (480MHz) to ±REF\_CLKOUT, nREF\_CLKOUT)



**Differential Input Level**







**Output Isolation**

### **Parameter Measurement Information, continued**



**LVDS Output Duty Cycle/Pulse Width/Period**



**Differential Output Voltage Setup**



**PLL Lock Time**



**LVDS Output Rise/Fall Time**



**Offset Voltage Setup**

# **Applications Information**

#### **Recommendations for Unused Input and Output Pins**

#### **Inputs:**

#### **LVCMOS Control Pins**

All control pins have internal pullups or pulldowns; additional resistance is not required but can be added for additional protection. A 1kΩ resistor can be used.

#### **Outputs:**

#### **LVDS Outputs**

All unused LVDS output pairs can be either left floating or terminated with 100Ω across. If they are left floating, we recommend that there

#### **Wiring the Differential Input to Accept Single-Ended Levels**

*Figure1* shows how a differential input can be wired to accept single ended levels. The reference voltage  $V_1 = V_{DD}/2$  is generated by the bias resistors R1 and R2. The bypass capacitor (C1) is used to help filter noise on the DC bias. This bias circuit should be located as close to the input pin as possible. The ratio of R1 and R2 might need to be adjusted to position the  $V_1$ in the center of the input voltage swing. For example, if the input clock swing is 2.5V and  $V_{DD} = 3.3V$ , R1 and R2 value should be adjusted to set  $V_1$  at 1.25V. The values below are for when both the single ended swing and  $V_{DD}$  are at the same voltage. This configuration requires that the sum of the output impedance of the driver (Ro) and the series resistance (Rs) equals the transmission line impedance. In addition, matched termination at the input will attenuate the signal in half. This can be done in one of two ways. First, R3 and R4 in parallel should equal the transmission line impedance.

For most 50Ω applications, R3 and R4 can be 100Ω. The values of the resistors can be increased to reduce the loading for slower and weaker LVCMOS driver. When using single-ended signaling, the noise rejection benefits of differential signaling are reduced. Even though the differential input can handle full rail LVCMOS signaling, it is recommended that the amplitude be reduced. The datasheet specifies a lower differential amplitude, however this only applies to differential signals. For single-ended applications, the swing can be larger, however  $V_{|L}$  cannot be less than -0.3V and  $V_{|H}$  cannot be more than  $V_{DD}$  + 0.3V. Though some of the recommended components might not be used, the pads should be placed in the layout. They can be utilized for debugging purposes. The datasheet specifications are characterized and guaranteed by using a differential signal.



**Figure 1. Recommended Schematic for Wiring a Differential Input to Accept Single-ended Levels**

### **3.3V LVPECL Clock Input Interface**

The REF\_CLK/nREF\_CLK accepts LVPECL, LVDS, HCSL and other differential signals. Both differential signals must meet the  $V_{PP}$  and V<sub>CMR</sub> input requirements. *Figures 2A to 2D* show interface examples for the REF\_CLK/nREF\_CLK input driven by the most common driver



**Figure 2A. REF\_CLK/nREF\_CLK Input Driven by a 3.3V LVPECL Driver**



**Figure 2C. REF\_CLK/nREF\_CLK Input Driven by a 3.3V LVDS Driver**

types. The input interfaces suggested here are examples only. If the driver is from another vendor, use their termination recommendation. Please consult with the vendor of the driver component to confirm the driver termination requirements.



**Figure 2B. REF\_CLK/nREF\_CLK Input Driven by a 3.3V LVPECL Driver with AC Couple**



**Figure 2D. REF\_CLK/nREF\_CLK Input Driven by a 3.3V HCSL Driver**

#### **LVDS Driver Termination**

A general LVDS interface is shown in *Figure 3A.* Standard termination for LVDS type output structure requires both a 100Ω parallel resistor at the receiver and a 100Ω differential transmission line environment. In order to avoid any transmission line reflection issues, the 100Ω resistor must be placed as close to the receiver as possible. IDT offers a full line of LVDS compliant devices with two types of output structures: current source and voltage source. The standard

termination schematic as shown in Figure 3A can be used with either type of output structure. If using a non-standard termination, it is recommended to contact IDT and confirm if the output is a current source or a voltage source type structure. In addition, since these outputs are LVDS compatible, the amplitude and common mode input range of the input receivers should be verified for compatibility with the output.



**LVDS Driver Termination**

#### **VFQFN EPAD Thermal Release Path**

In order to maximize both the removal of heat from the package and the electrical performance, a land pattern must be incorporated on the Printed Circuit Board (PCB) within the footprint of the package corresponding to the exposed metal pad or exposed heat slug on the package, as shown in *Figure 4.* The solderable area on the PCB, as defined by the solder mask, should be at least the same size/shape as the exposed pad/slug area on the package to maximize the thermal/electrical performance. Sufficient clearance should be designed on the PCB between the outer edges of the land pattern and the inner edges of pad pattern for the leads to avoid any shorts.

While the land pattern on the PCB provides a means of heat transfer and electrical grounding from the package to the board through a solder joint, thermal vias are necessary to effectively conduct from the surface of the PCB to the ground plane(s). The land pattern must be connected to ground through these vias. The vias act as "heat pipes". The number of vias (i.e. "heat pipes") are application specific

and dependent upon the package power dissipation as well as electrical conductivity requirements. Thus, thermal and electrical analysis and/or testing are recommended to determine the minimum number needed. Maximum thermal and electrical performance is achieved when an array of vias is incorporated in the land pattern. It is recommended to use as many vias connected to ground as possible. It is also recommended that the via diameter should be 12 to 13mils (0.30 to 0.33mm) with 1oz copper via barrel plating. This is desirable to avoid any solder wicking inside the via during the soldering process which may result in voids in solder between the exposed pad/slug and the thermal land. Precautions should be taken to eliminate any solder voids between the exposed heat slug and the land pattern. Note: These recommendations are to be used as a guideline only. For further information, please refer to the Application Note on the Surface Mount Assembly of Amkor's Thermally/ Electrically Enhance Leadframe Base Package, Amkor Technology.



**Figure 4. P.C. Assembly for Exposed Pad Thermal Release Path – Side View (drawing not to scale)**

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#### **Schematic Example**

*Figure 5* shows an example of IDT8V44N003I application schematic. Input and output terminations shown are intended as examples only and may not represent the exact user configuration.

As with any high speed analog circuitry, the power supply pins are vulnerable to noise. To achieve optimum jitter performance, power supply isolation is required. The IDT8V44N003I provides separate power  $V_{DD}$  and  $V_{DDA}$  power supplies to isolate from coupling into the internal PLL.

In order to achieve the best possible filtering, it is recommended that the placement of the filter components be on the device side of the PCB as close to the power pins as possible. If space is limited, the

0.1uF capacitor in each power pin filter should be placed on the device side of the PCB and the other components can be placed on the opposite side.

Power supply filter recommendations are a general guideline to be used for reducing external noise from coupling into the devices. The filter performance is designed for wide range of noise frequencies. This low-pass filter starts to attenuate noise at approximately 10kHz. If a specific frequency noise component is known, such as switching power supply frequencies, it is recommended that component values be adjusted and if required, additional filtering be added. Additionally, good general design practices for power plane voltage stability suggests adding bulk capacitances in the local area of all devices.



#### **Figure 5. IDT8V44N003I Application Schematic**

### **Power Considerations**

This section provides information on power dissipation and junction temperature for the IDT8V44N003I. Equations and example calculations are also provided.

#### **1. Power Dissipation.**

The total power dissipation for the IDT8V44N003I is the sum of the core power plus the analog power plus the power dissipated in the load(s). The following is the power dissipation for  $V_{DD} = 3.3V + 5\% = 3.465V$ , which gives worst case results.

 $Power (core)_{MAX} = V_{DD\_MAX} * (I_{DD\_MAX} + I_{DDA\_MAX}) = 3.465V * (136mA + 17mA) = 530.145mW$ 

#### **2. Junction Temperature.**

Junction temperature, Tj, is the temperature at the junction of the bond wire and bond pad directly affects the reliability of the device. The maximum recommended junction temperature is 125°C. Limiting the internal transistor junction temperature, Tj, to 125°C ensures that the bond wire and bond pad temperature remains below 125°C.

The equation for Tj is as follows: Tj =  $\theta_{JA}$  \* Pd\_total + T<sub>A</sub>

 $Tj$  = Junction Temperature

 $\theta_{JA}$  = Junction-to-Ambient Thermal Resistance

Pd\_total = Total Device Power Dissipation (example calculation is in section 1 above)

 $T_A$  = Ambient Temperature

In order to calculate junction temperature, the appropriate junction-to-ambient thermal resistance  $\theta_{JA}$  must be used. Assuming no air flow and a multi-layer board, the appropriate value is 43.7°C/W per Table 6 below.

Therefore, T<sub>i</sub> for an ambient temperature of 85°C with all outputs switching is:

 $85^{\circ}$ C + 0.530W  $*$  43.7°C/W = 108.2°C. This is below the limit of 125°C.

This calculation is only an example. Tj will obviously vary depending on the number of loaded outputs, supply voltage, air flow and the type of board (multi-layer).

#### Table 6. Thermal Resistance  $θ<sub>JA</sub>$  for 32 Lead VFQFN, Forced Convection



# **Reliability Information**

#### **Table 7.** θ**JA vs. Air Flow Table for a 32 Lead VFQFN**



#### **Transistor Count**

The transistor count for IDT8V44N003I is: 47,632

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**Package Outline and Package Dimensions**





# **Ordering Information**

#### **Table 8. Ordering Information**



NOTE: Parts that are ordered with an "G" suffix to the part number are the Pb-Free configuration and are RoHS compliant.



# **Revision History Sheet**





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